#### THE VIBRATION RESPONSE OF A PANEL TO AN ACOUSTIC PRESSURE FIELD

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#### Introduction

Consider an acoustic pressure field which excites a homogenous panel. Assume that the pressure field has random incidence upon the panel.

As an example, a satellite is mounted inside of a launch vehicle nosecone fairing. The satellite's solar panels must withstand the liftoff acoustic field. The fairing attenuates a great deal of this energy. Nevertheless, a portion of the acoustical energy is transmitted to the satellite.

The purpose of this report is to derive a relationship between the acoustic pressure and the panel vibration response.

#### **Critical Frequency**

The critical frequency is the frequency at which the airborne acoustic wavelength matches the panel bending wavelength. The critical frequency  $f_{\rm c}$  for a homogeneous panel is

$$f_{c} \approx \frac{c^{2}}{1.8 c_{L} h} \tag{1}$$

where

c is the speed of sound in the surrounding air medium

 $c_L$  is the longitudinal wave velocity

h is the panel thickness

Equation (1) is taken from Reference 1, chapter 6, equation (56a).

#### Panel Velocity Response to Acoustic Pressure

Let  $V_{\mbox{RMS}}$  be the velocity root-mean-square.

Let  $P_{RMS}$  be the pressure root-mean-square.

The velocity and pressure are related by the following semi-empirical equation.

$$\left[V_{RMS}\right]^2 = \beta \left[P_{RMS}\right]^2 \tag{2}$$

Equation (2) is taken from Reference 1, chapter 8.

Note that each term in equation (2) is a function of frequency.

The coefficient  $\beta$  is

$$\beta = \begin{cases} \frac{1}{2\pi^2 f^2 m^2} \left[ 1 - \frac{\rho c}{\pi f m} \arctan\left(\frac{\pi f m}{\rho c}\right) \right], & \text{for } f < f_C \end{cases}$$

$$\frac{c^2}{8\pi f^2 m^2 c_B^2 \eta}, & \text{for } f \ge f_C \end{cases}$$
(3)

where

f is the excitation frequency

m is the mass per area

c is the speed of sound in the surrounding air

ρ is the mass per volume of the surrounding air

C<sub>B</sub> is the phase speed of the bending waves in the panel

 $\eta$  is the loss factor

Equation (3) is taken from Reference 1, chapter 8, section c for frequencies below the critical frequency.

Equation (3) is derived from Reference 1, chapter 8, section d, equations (101) through (103) for frequencies above the critical frequency.

Note that the phase speed  $C_B$  and the loss factor  $\eta$  each vary with frequency.

### Panel Phase Speed

Consider a panel with thickness h and a longitudinal wave velocity of C<sub>L</sub>. The longitudinal velocity is a constant for a given material. The phase speed is

$$C_{\mathbf{B}} \approx \sqrt{1.8 \ C_{\mathbf{L}} h f} \tag{4}$$

Equation (4) is taken from Reference 1, chapter 3.

#### Mass Law

Equation (2) essentially follows the "mass law" below the critical frequency. A doubling of either the mass density or the frequency causes the velocity to decrease to one-half its value, which is equivalent to a 6 dB drop.

Equation (2) is complicated above the critical frequency due to the variation of the phase speed and loss factor with frequency.

#### Loss Factor

The loss factor  $\eta$  is an empirical parameter. The loss factor is assumed to be due mainly to acoustic radiation above the critical frequency.

A mean loss factor curve for aluminum panels is shown in Figure 1. The frequency scale is normalized in terms of the critical frequency. The panels were suspended from a frame by elastic cords such that the boundary conditions were essentially free around the perimeter. The data was taken from two panels. One panel was 1/4 inch thick. The other was 1/2 inch thick. Each panel was 4.0 by 6.5 feet.

The data in Figure 1 is thus approximate data for a particular material, geometry, and boundary condition case. Loss factor measurements on a particular structure of interest must thus be taken in order to accurately use the calculation methods in this report.

# LOSS FACTORS FOR HOMOGENEOUS ALUMINUM PANELS FREE BOUNDARY CONDITION ON ALL SIDES

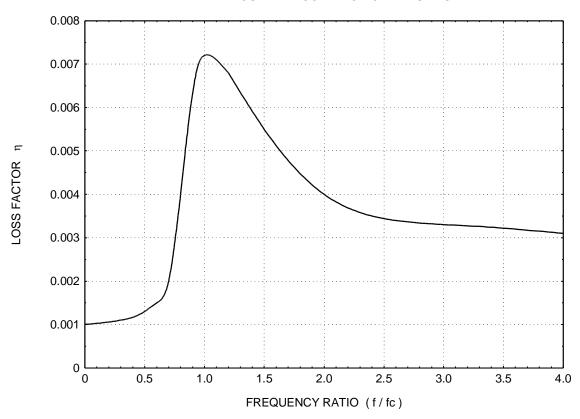


Figure 1.

# Power Spectrum Format

Acoustic pressure fields are typically represented in one-third octave band power spectra.

Let V PS be the velocity power spectrum.

Let P<sub>PS</sub> be the pressure power spectrum.

Equation (2) can be modified as follows

$$[V_{PS}] = \beta [P_{PS}] \tag{5}$$

The acceleration is often of greater interest than velocity for structural vibration.

Let A <sub>PS</sub> be the acceleration power spectrum.

$$\left[A_{PS}\right] = \beta \left[2\pi f\right]^2 \left[P_{PS}\right] \tag{6}$$

# Reference Data

The parameter pc is called the "characteristic impedance." The values for air are shown in Table 1. The speed of sound for gases and solid is given in Tables 2 and 3, respectively.

Table 1. Characteristic Impedance ρc						
	Impedance	Impedance				
Gas and Temperature	( Pa · s/ m )	$(lbf \cdot s / ft^3)$				
Air at 0° C	428	2.73				
Air at 20° C	415	2.64				

Table 2. Gases at a pressure of 1 atmosphere									
Gases	Molecular	Temperature	Density	Ratio of	Speed of				
	Mass	(°C)	$(kg/m^3)$	Specific	Sound				
	(kg/kgmole)		(8, )	Heats	(m/sec)				
Air	28.97	0	1.293	1.402	332				
Air	28.97	20	1.21	1.402	343				
Oxygen (O <sub>2</sub> )	32.00	0	1.43	1.40	317				
Hydrogen (H <sub>2</sub> )	2.016	0	0.09	1.41	1270				
Steam	ı	100	0.60	1	404.8				

Table 3. Solids							
					Speed of Sound		
					(m/sec)		
Solid	Density	Elastic	Shear	Poisson's			
	$(kg/m^3)$	Modulus	Modulus	Ratio	Bar	Bulk	
	(mg/mr/)	(Pa)	(Pa)				
Aluminum	2700	7.0 (10 <sup>10</sup> )	2.4 (10 <sup>10</sup> )	0.33	5100	6300	
Brass	8500	10.4 (10 <sup>10</sup> )	3.8 (10 <sup>10</sup> )	0.37	3500	4700	
Copper	8900	12.2 (10 <sup>10</sup> )	4.4 (10 <sup>10</sup> )	0.35	3700	5000	
Steel	7700	19.5 (10 <sup>10</sup> )	8.3 (10 <sup>10</sup> )	0.28	5050	6100	
Ice	920	-	-	-	-	3200	
Glass (Pyrex)	2300	6.2 (10 <sup>10</sup> )	2.5 (10 <sup>10</sup> )	0.24	5200	5600	

# <u>Reference</u>

1. L. Cremer and M. Heckl, Structure-Borne Sound, Springer-Verlag, New York, 1988.